# Performance of radiation-based reference evapotranspiration equation developed for Indian sub-humid conditions

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## ABSTRACT

In this study, asite-specific radiation based equation for estimating reference evapotranspiration  $(ET_{.0})$  was developed and its performance was statistically analysed in comparison to widely accepted FAO Penman-Monteith (FAO-56 PM) model and four radiation-based  $ET_{.0}$  methods for sub-humid Hazaribagh region of Jharkhand state. The equation was developed with daily values of incoming solar radiation in conjunction with air temperature (minimum and maximum) by considering daily FAO-56 PM  $ET_{0}$  values as index with weather dataset of 15 years (1990-2004). The performance of developed equation validated with eight years (2005-2012) daily weather dataset revealed that it estimated  $ET_{0}$  values better than other radiation-based methods. The respective higher and lower values of agreement index and root mean square error with FAO-56 PM  $ET_{0}$  values during validation period confirms efficacy of developed equation whose performance tested at another Indian sub-humid location (Pantnagar) confirmed its suitability as well. Considering the limitations associated with reliability and availability of weather data  $ET_{0}$  in sub-humid climatic conditions if FAO-56 PM model cannot be used due to non-availability of required weather parameters at a location.

Keywords: Radiation-based equation, reference evapotranspiration, sub-humid, Hazaribagh, Pantnagar

Under diminishing water resources, increasing consumption and pollution, water available for irrigation is shrinking. In Indian conditions, distribution of precipitation (main source of water for crop production) is very uneven and uncertain. For effective water management under water scarce situation, farmers have to opt proper irrigation scheduling for which it is essential to know environmental demand for surface water whose loss occurs primarily through evapotranspiration (ET). Accordingto Hansen et al. (1980), ET is the amount of water returned to the atmosphere through evaporation (moisture loss from soil, standing water etc.) and transpiration (biological use and release of water by vegetation). If environmental demand for water (ET) exceeds the water available to plant through precipitation or stored in the soil, then transpiration may cease resulting in crop loss and, therefore, reliable estimates of ET is essentially required (Watson and Burnett, 1995).

Reference evapotranspiration  $(ET_0)$  is a modification of ET concept that provides a standard crop (a short, clipped grass) with an unlimited water supply so that a user can calculate maximum evaporative demand from that surface for a given day. This value, adjusted for a particular crop is its consumptive use (or demand) and its deficit represent that component of consumptive use that goes unfilled, either by precipitation or by soil moisture during the given time period (Allen *et al.*, 1998). The information about  $ET_0$  is required for crop production, environment assessment, irrigation scheduling, water resources management etc. Since its direct measurement using lysimeter is cumbersome, challenging, time consuming the most common procedure to estimate  $ET_0$  is from observed meteorological variables (Dingman, 1994; Allen *et al.*, 1998; Barnett *et al.*, 1998).

The International Commission for Irrigation and Drainage and the Food and Agriculture Organization (FAO) of the United Nations Expert Consultation on Revision of Methodologies for Crop Water Requirements (Smith *et al.*, 1991) recommended FAO Penman–Monteith (FAO-56 PM) model as standard to estimate  $ET_0$  which requires solar radiation, wind speed, air temperature and humidity data, however, all these input variables for a given location especially in developing countries, like India, may not be available where data quality and difficulties in gathering all necessary weather parameters can present serious limitations. When climate data required for estimating  $ET_0$ 

with FAO-56 PM model are not available or reliable for a location, empirical or simplified  $ET_0$  equations requiring fewer parameters can be used.

Keeping in view the above, the present study was taken up with objectives: (i) to develop a radiation-based  $ET_0$  equation considering FAO-56 PM  $ET_0$  model as index; (ii) to evaluate the performance of developed equation in comparison to radiation-based  $ET_0$  methods; and (iii) to validate developed equation at another sub-humid location.

## **MATERIALS AND METHODS**

#### Study area and weather dataset

Daily weather dataset for a period of 23 years (1 January 1990 to 31 December 2012), obtained for subhumid Hazaribagh (23.89°N latitude, 85.5°E longitude, 604.00 m above m.s.l.) region of Jharkhand state was used in this study. The study area experiences three distinct seasons i.e., summer (February-May), monsoon (June-September) and winter (October-January) with an average annual rainfall of about 783 mm.

#### Reference evapotranspiration estimation

In this study, FAO-56 PM model was chosen as index to compute daily  $ET_0$  values, expressed mathematically (Smith *et al.*, 1992) as:

$$ET_{0} = \frac{0.408 \,\Delta(R_{n}-G) + \gamma(\frac{900}{T_{dv} + 275}) U_{2}(e_{s}-e_{a})}{\Delta + \gamma(1+0.34U_{2})} \dots (1)$$

where  $ET_0$  is reference evapotranspiration (mm day<sup>-1</sup>);  $R_n$  is net radiation at crop surface (MJm<sup>-2</sup>day<sup>-1</sup>); G is soil heat flux density (MJm<sup>-2</sup>day<sup>-1</sup>);  $T_{av}$  is mean daily air temperature (°C);  $U_2$  is wind speed at 2 m height (msec<sup>-1</sup>);  $e_s$  is saturation vapour pressure (kPa);  $e_a$  is actual vapour pressure (kPa);  $e_s$ - $e_a$  is saturation vapour pressure deficit (kPa); y is slope of vapour pressure curve (kPa°C<sup>-1</sup>); and ã is psychrometric constant (kPa°C<sup>-1</sup>). Since soil heat flux density (G) has relatively a small value, it was considered zero for daily calculations in accordance with Allen *et al.* (1998).

In addition to FAO-56PM model, four radiation-based  $ET_0$  methods namely, FAO24-Radiation (Doorenbos and Pruitt, 1977), Jensen–Haise (1963), McGuinness-Bordne (1972) and Priestley-Taylor (1972) were considered to evaluate the performance of developed equation.

## Development of radiation-based ET, equation

A radiation-based ET<sub>o</sub>equation for sub-humid

Hazaribagh region of Jharkhand state was developed with Multiple Linear Regression (MLR) approach by considering 65% of daily weather dataset (1990-2004) for calibration, whereas, remaining 35% dataset (2005-2012) was used for validating it. The MLR approach was used as linear form presumes that each parameter impacts  $ET_0$  independent of other parameters and it reduces the requirement of input parameters. For determining coefficients of developed equation, daily FAO-56 PM  $ET_0$  values were taken as dependent variable, whereas, daily values of  $R_s$ ,  $T_{max}$  and  $T_{min}$  were used as independent variables.

#### Statistical analysis

To ensure rigorous comparison of developed equation and considered methods to evaluate their performance in comparison to FAO-56 PM model, an extended analysis in terms of statistical indices namely, Agreement index (D), Root Mean Square Error (RMSE), Coefficient of determination ( $R^2$ ) and Standard Error of Estimates (SEE) was undertaken with the help of Microsoft<sup>TM</sup> Excel® as computing tool. On the basis of literature reviewed, higher values of D and R<sup>2</sup> (near to 1.00) and values near to 0.00 for RMSE and SEE were considered "good". The quantification of under- and over-estimation of developed equation and radiation-based methods as compared to FAO-56 PM model was done in terms of their ratio (ET<sub>0</sub> method/ET<sub>0</sub>FAO-56 PM)and its value near to 1.00 was considered "good".

## **RESULTS AND DISCUSSION**

#### Radiation-based ET<sub>o</sub> equation

The first-order MLR equation to estimate values of FAO-56 PM ET<sub>0</sub> (mm day<sup>-1</sup>) as a function of R<sub>s</sub> (MJ m<sup>-2</sup> day<sup>-1</sup>), maximum air temperature (T<sub>max</sub>, °C) and minimum air temperature (T<sub>min</sub>, °C) was determined as:

 $ET_0 = -5.7547 + 0.1664 R_s + 0.2348 T_{max} - 0.0015 T_{min} \dots (2)$ 

For calibrating this equation with 5479 number of daily observations over 15 years period (1990-2004), the curvilinear regression (Fig. 1) was found significant ( $R^2 = 0.903$ ).

#### Performance of equation during calibration period

The performance of developed equation was evaluated by comparing its daily and monthly estimates with those obtained with FAO-56 PMmodel and considered methods in terms of statistical indices and average ratio of  $ET_0$  method/ $ET_0$ FAO-56 PM.For monthly comparisons, daily  $ET_0$  values averaged over one month period were plotted



Fig. 2: Regression analysis for validating developed ET equation

against calculated FAO-56 PM values.

The relative performance of developed equation for calibration period (1990-2004) on daily and monthly basis (Table 1) reveals that on daily basis, highest values of D (0.96) and R<sup>2</sup> (0.88); lowest values of RMSE (0.69 mm day<sup>-1</sup>) and SEE (0.61 mm day<sup>-1</sup>) were obtained with developed equation. Similarly, the value of ratio as 1.01 obtained with developed equation extends its superiority over other methods.FromTable 1, it is clear that the developed equation performed best on both daily and monthly basis.

#### Validation of the equation

Eight years of daily weather dataset, consisting of 2922 observations was used to validate the developed equation. The comparison of daily  $ET_0$  values estimated using developed equation with that of radiation-based methods on daily and monthly basis for validation period (2005-2012) is presented in Table 2.

From Table 2, it is clear that  $ET_0$  values calculated with developed equation followed FAO-56 PM values closely

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Equation / Methods	D	RMSE	R <sup>2</sup>	SEE	Ratio
		Daily ba	sis		
Developed equation	0.96	0.69	0.88	0.61	1.01
FAO24-Radiation	0.93	0.98	0.83	0.78	1.17
Jensen-Haise	0.81	1.76	0.83	0.74	0.56
McGuiness-Bordne	0.71	2.29	0.49	1.44	1.54
Priestley-Taylor	0.87	4.20	0.78	2.43	0.97
		Monthly b	pasis		
Developed equation	0.99	1.76	0.96	1.36	1.01
FAO24-Radiation	0.94	3.29	0.91	2.20	1.18
Jensen-Haise	0.80	7.12	0.92	2.03	0.58
McGuiness-Bordne	0.73	9.36	0.60	6.11	1.47
Priestley-Taylor	0.87	4.20	0.78	2.43	0.97

 Table 1:Comparative performance of developed equation and radiation-based methods versus FAO-56 PM model during calibration period (1990-2004) at Hazaribagh

 $D = A greement index, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mmday^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Squar$ 

SEE = Standard Error of Estimates (mm day<sup>-1</sup>), Ratio = Ratio of ET<sub>0</sub> method/ET<sub>0</sub>FAO-56 PM.

 Table 2: Comparative performance of developed equation and radiation-based methods versus FAO-56 PM model during validation period (2005-2012) at Hazaribagh

Equation / Methods	D	RMSE	$\mathbb{R}^2$	SEE	Ratio
		Daily ba	sis		
Developed equation	0.96	0.66	0.90	0.57	1.06
FAO24-Radiation	0.92	1.01	0.84	0.73	1.20
Jensen-Haise	0.85	1.43	0.84	0.73	0.62
McGuiness-Bordne	0.69	2.30	0.56	1.30	1.58
Priestley-Taylor	0.93	2.83	0.87	0.59	1.02
		Monthly b	pasis		
Developed equation	0.99	1.80	0.97	1.24	1.07
FAO24-Radiation	0.92	3.66	0.90	2.25	1.21
Jensen-Haise	0.83	5.72	0.91	2.13	0.64
McGuiness-Bordne	0.69	9.58	0.68	5.37	1.52
Priestley-Taylor	0.93	2.83	0.87	1.94	1.02

 $D = A greement index, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determinatio$ 

SEE = Standard Error of Estimates (mm day<sup>-1</sup>), Ratio = Ratio of  $ET_0$  method/ $ET_0$ FAO-56 PM.

demonstrating that it can be used to estimate  $ET_0$  with reasonable accuracy. On daily basis, developed equation performed best with highest values of D (0.96) and R<sup>2</sup> (0.90); lowest values of RMSE (0.66 mm day<sup>-1</sup>) and SEE (0.57mm day<sup>-1</sup>) in comparison to radiation-based methods, whereas, on monthly basis, lowest average value of SEE (1.24mm day<sup>-1</sup>) in comparison to McGuinness-Bordne (5.37mm day<sup>-1</sup>), FAO24-Radiation (2.25mm day<sup>-1</sup>), Jensen-Haise (2.13mm day<sup>-1</sup>) and Priestley-Taylor (1.94mm day<sup>-1</sup>) methods confirms its better performance.On daily basis, the average ratio of  $ET_0$  method/ $ET_0$ FAO-56 PM with developed equation was obtained as 1.06, whereas, its highest value (1.58) was obtained with McGuinness-Bordne method. From Fig. 2, it is evident that  $ET_0$  values calculated by developed equation

Performance indicator	Developed equation	FAO24- Radiation	Jensen- Haise	McGuiness- Bordne	Priestley- Taylor	
Daily SEE	0.57	0.73	0.73	1.30	0.59	
Monthly SEE	1.24	2.25	2.13	5.37	1.94	
Averageratio	1.06	1.20	0.62	1.58	1.02	

SEE = Standard Error of Estimates (mm day<sup>-1</sup>)

 Table 4: Comparative performance of developed equation and radiation-based methods versus FAO-56 PM model during study period (1990-2012) at Hazaribagh

Equation / Methods	D	RMSE	$\mathbb{R}^2$	SEE	Ratio
		Dailyba	sis		
Developed equation	0.96	0.68	0.88	0.60	1.02
FAO24-Radiation	0.92	0.99	0.83	0.76	1.18
Jensen-Haise	0.82	1.64	0.83	0.73	0.59
McGuiness-Bordne	0.71	2.29	0.52	1.39	1.56
Priestley-Taylor	0.87	1.05	0.71	0.68	1.00
		Monthly b	pasis		
Developed equation	0.99	1.77	0.97	1.32	1.03
FAO24-Radiation	0.94	3.42	0.91	2.21	1.19
Jensen-Haise	0.81	6.63	0.92	2.06	0.60
McGuiness-Bordne	0.71	9.44	0.63	5.85	1.49
Priestley-Taylor	0.90	3.72	0.81	2.26	0.99

D = Agreement index, RMSE = Root Mean Square Error (mm day<sup>-1</sup>), R<sup>2</sup> = Coefficient of determination,

SEE = Standard Error of Estimates (mm day<sup>-1</sup>), Ratio = Ratio of  $ET_0$  method/ $ET_0$ FAO-56 PM.

were strongly correlated ( $R^2=0.918$ ) with that of the FAO-56 PM model.

The values of SEE and ratio for developed equation and radiation-based methods on daily and monthly basis for individual years during validation period (2005-2012) are presented in Table 3. From Table 3, it is clear that developed equation resulted in lowest average SEE of daily estimate (0.57 mm day<sup>-1</sup>), whereas, its value for radiation-based methods was found much higher ranging from 0.73 to 1.30 mm day<sup>-1</sup>. Ingeneral, the performance of developed equation was found better at both the timescales.

#### Performance during study period (1990-2012)

The statistical performance of developed equation in comparison to radiation-based methods during study period (Table 4) reveals that on both daily and monthly basis,  $ET_0$  values calculated with developed equation were strongly correlated with that of FAO-56 PM model with highest values of R<sup>2</sup>(0.99 and 0.97) and D (0.96 and 0.88) and lowest

daily and monthly SEE values as  $0.60 \,\text{mm}$  day<sup>-1</sup> and  $1.32 \,\text{mm}$  day<sup>-1</sup> respectively.

From Table 4, it is clear that the ratio of  $ET_0$  method/ ET\_0FAO-56 PM with developed equation at both the time scales was obtained near to 1.00. It was also observed that McGuinness-Bordneand Jensen-Haise methods respectively gave almost 50 percent higher and 40 percent lower valueson both daily and monthly basis in comparison to its "good" value of 1.00.

#### Performance at another sub-humid location

The performance of developed equation was further evaluated at another sub-humid location, Pantnagar (29°N latitude, 79.3°E longitude, 243.80 m above m.s.l.), located in the foothills of the great Himalayas in Uttarakhand and is presented in Table 5. The continuous daily full weather dataset for 24 year duration (1990-2013) obtained from meteorological observatory situated in the premises of Crop Research Centre of the Govind Ballabh Pant University of

(1990-2013)					
Equation / Methods	D	RMSE	$\mathbb{R}^2$	SEE	Ratio
		Dailyba	sis		
Developed equation	0.98	0.84	0.91	0.64	1.00
FAO24-Radiation	0.95	0.86	0.89	0.68	1.17
Jensen-Haise	0.89	1.48	0.82	0.80	0.62
McGuiness-Bordne	0.75	2.33	0.66	1.38	1.60
Priestley-Taylor	0.94	0.88	0.81	0.73	1.01
		Monthly b	pasis		
Developed equation	0.99	2.78	0.97	1.68	1.00
FAO24-Radiation	0.96	2.83	0.95	1.77	1.18
Jensen-Haise	0.86	5.74	0.89	2.34	0.64
McGuiness-Bordne	0.75	9.44	0.80	5.05	1.53
Priestley-Taylor	0.96	2.80	0.88	2.44	1.00

 Table 5: Comparative performance of developed equation and radiation-based methods versus FAO-56 PM model at Pantnagar (1990-2013)

 $D = A greement index, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determination, RMSE = Root Mean Square Error (mm day^{-1}), R^2 = Coefficient of determinatio$ 

SEE = Standard Error of Estimates (mm day-1), Ratio = Ratio of  $ET_0$  method/ $ET_0$  FAO-56 PM.

Agriculture & Technology, Pantnagar (Uttarakhand) was used in this study.

From Table 5, it is clear that in comparison to radiationbased methods, developed equation performed better as it produced highest values of D (0.98 and 0.91) and R<sup>2</sup> (0.99 and 0.97); lowest values of RMSE (0.84 and 0.64 mm day<sup>-1</sup>) and SEE (2.78 and 1.68 mm day<sup>-1</sup>) and ratio (1.00 and 1.00) on daily and monthly basis respectively which confirms that developed equation can be used successfully to estimate ET<sub>0</sub> at other sub-humid locations.

## CONCLUSIONS

A site-specific radiation-based  $ET_0$  equation was developed with multiple linear regression approach for subhumid Hazaribagh region of Jharkhand statewith daily weather dataset of 15 years duration (1990-2004), whereas, eight years (2005-2012) of daily weather datasetwas used to validate it. The estimates of daily and monthly  $ET_0$  values obtained with developed equation were foundvery close to that of the FAO-56 PM model in comparison to radiationbased methods.

The performance of developed equation evaluated at another Indian sub-humid location (Pantnagar, Uttarakhand) with daily weather dataset of 24 years (1990-2013) confirmed that it can be utilized as a practical method to estimate  $ET_0$  successfully in Indian sub-humid regions if standard FAO-56 PM model cannot be used due to limitations associated with availability and reliability of required meteorological

dataset. The evaluation of developed equation is recommended at other sub-humid locations as well.

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